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Anti-pick-up Coatings for furnace rolls in CALs & CGLs



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Design of anti-pick-up coatings

The design of pick-up resistant coating solutions were outlined according to the different pick-up type and the formation mechanism at low and high temperatures :

- **At low temperatures: mechanical bonding and sintering of Fe particles** induced by coating's surface roughness and by metal friction due to the presence of a metallic binder in cermet coatings.  **Coatings for cooling & overageing sections.**
- **At high temperatures: Chemical interaction** of MnO/SiO_2 (from steels) due to the presence of Cr_2O_3 / Al_2O_3 (from coatings) forming sticky spinels.  **Coatings for heating & soaking sections.**
- For both applications, **hardness** must be improved for avoiding **wear defects**.

Roll coatings for low temperature applications

- Chemical interactions between rolls and strip oxides are not an issue: kinetics is too slow at temperatures $< 500^{\circ}\text{C}$;
- Mechanical interactions occur: coating's surface roughness should be as low as possible;
- Sintering between Fe debris and the metal binder in the coating can occur making Fe pick-ups very adherent: the amount of metal in the coating must be limited.



Coatings must be smooth, dense, with no or lowest possible metal and characterized by a high hardness.

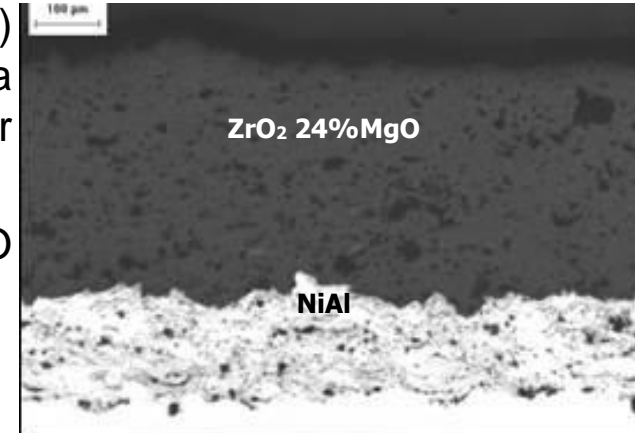
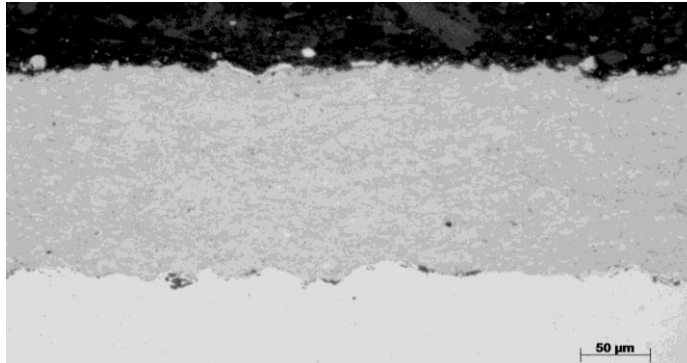
Roll coatings for low temperature applications

WC-CrC-Ni (73%-20%-7%) cermet coating has a low metal binder.

Cermet coatings deposited by High Velocity Air Fuel (HVOF) instead of High Velocity Oxygen Fuel (HVOF). **HVOF** can form a more uniform and finer dispersion of ceramics in a denser metallic matrix → higher hardness

Ceramic oxide coatings with bond coats, i.e. $\text{ZrO}_2\text{-MgO}$ coating

Measurement	Value
Thickness (μm)	170
Porosity (%)	0,35
Oxides (%)	0,2
Microhardness (HV 0.3)	1200

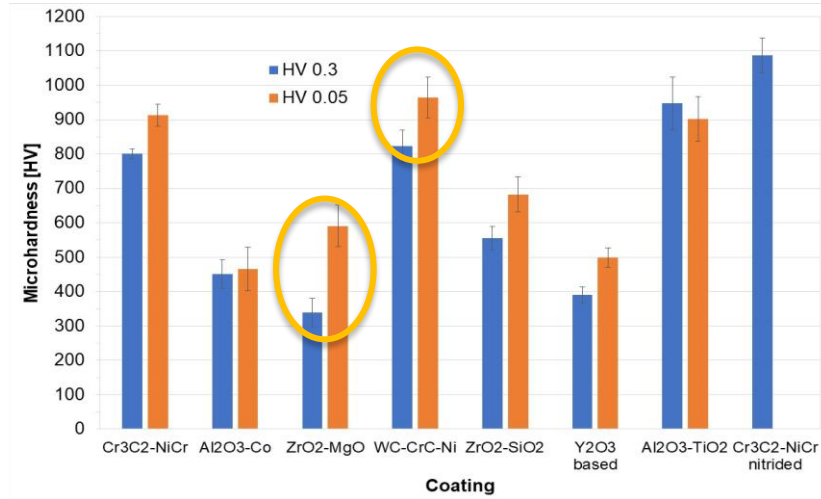


	substrate	Bond-coat	Top coat
	AISI 304	NiAl	zirconia
CTE	$17 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$	$13 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$	$11\text{-}13 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$

Roll coatings for low temperature applications

Coating type	Powder Composition
Cermet	Cr ₃ C ₂ in NiCr *
	Al ₂ O ₃ in Co (Cr, Al, Ni, Nb) *
	WC-CrC-Ni
	plasma nitrided Cr ₃ C ₂ - NiCr
Ceramic	ZrO ₂ -MgO
	ZrO ₂ -SiO ₂
	Al ₂ O ₃ TiO ₂
	Y ₂ O ₃ based

* reference coatings



- ZrO₂-MgO coating has a low hardness this behaviour rules out its application.
- The WC-CrC-Ni **cermet coating** deposited by HVAF having only 7% Ni and appropriate hardness appears to have the best characteristics. Moreover, it has a Co free metallic matrix that complies with the latest REACH regulations.

Roll coatings for high temperature applications



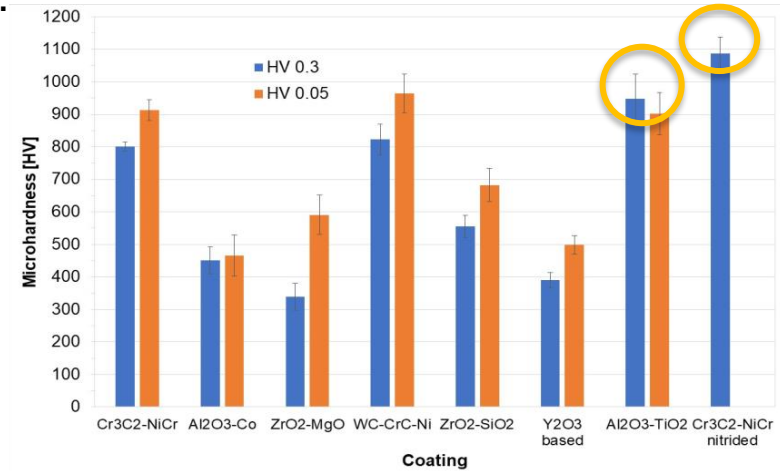
- Reactions between roll's surface oxides and strip oxides occur: to avoid the formation of sticky spinels, cermets with a metal binder containing mainly Ni and/or Co should be preferred.
- Cr and Nb (metallic or carbides) in the cermet coatings partly react in the typical annealing atmosphere (5-7% H_2/N_2 , $DP < -30^\circ C$) and are transformed into nitrides: it is suggested to directly incorporate in the coating stable nitrides by a controlled nitriding process aiming to transform partially Cr and CrC into CrN hard phases.
- ZrO_2 and other stable oxide coatings (i.e., Al_2O_3 , Y_2O_3) have shown not to react with the selective oxidation layer on steels.

Roll coatings for high temperature applications

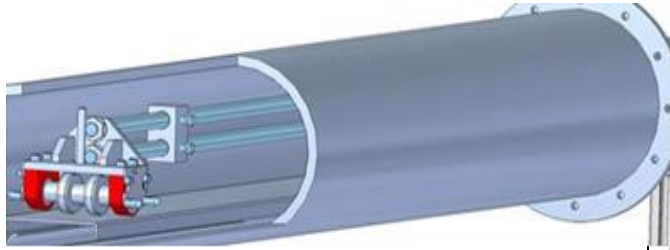
- **Cr₃C₂ - NiCr cermet coatings** submitted to a post-deposition **plasma nitriding** process in N₂ atmosphere for 24 h at 550°C for surface hardening.
- **Hard ceramic oxide coatings** with an alloy bond coat include, ZrO₂+(MgO or Y₂O₃), ZrO₂-SiO₂, Y₂O₃-based and Al₂O₃-TiO₂ coatings by plasma spraying with an innovative Water Plasma Torch (WPT).

Coating type	Powder Composition
Cermet	Cr ₃ C ₂ in NiCr *
	Al ₂ O ₃ in Co (Cr, Al, Ni, Nb) *
	WC-CrC-Ni
	plasma nitrided Cr ₃ C ₂ - NiCr
Ceramic	ZrO ₂ -MgO
	ZrO ₂ -SiO ₂
	Al ₂ O ₃ TiO ₂
	Y ₂ O ₃ based

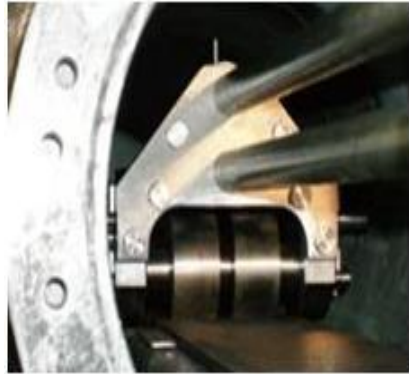
* reference coatings








Dynamic interaction testing at high temperatures



Dynamic interaction test rig for simulating HSS strip / roll coating interactions at 900°C under controlled annealing atmosphere: 5%H₂/N₂; Dew Point -30°C



				
Cr ₃ C ₂ -NiCr	Al ₂ O ₃ -Co matrix	WC-CrC-Ni	Nitride Cr ₃ C ₂ -NiCr	ZrO ₂ -MgO

- Cr₃C₂-NiCr and Al₂O₃-Co coatings form small randomly distributed pick-ups,
- nitride Cr₃C₂-NiCr, WC-CrC-Ni and ZrO₂-MgO coatings have few or no pick-ups
- Considerable powdering of the ceramic roll is due to its lower hardness, this behaviour rules out its application

NoStickRolls Project : rolls for testing



The coatings that appeared to have the aimed-for characteristics and hardness were selected for **laboratory tribological testing sequence** with the aim of identifying:

- the best ones for soaking zone application to be tested under **semi-industrial conditions** at the Roll Strip Interaction test bench
- the best one to coat rolls for **industrial trials** in the overageing zones in CAL & CGL.

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